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Supplement to *Wi*  
*Electrical Trader*, 14 *ja*

"TRADER" SERVICE SHEET  
**1227**



Appearance of the Ekco U243.

**EKCO A.M./**  
 3-band Table Rece

**E**MPLYING internal A.M. and F.M. aerials, the Ekco U243 is a 5-valve (plus rectifier and cathode ray tuning indicator) A.M./F.M. table receiver, designed for operation from A.C. or D.C. mains of 200-250 V, 40-100 c/s in the case of A.C. Total mains consumption is 60 watts. The waveband ranges are: A.M., 192-550m, 983-2,027m; F.M., 87-100 Mc/s.  
 Release date and original price: April, 1955, £19 16s 2d.

**CIRCUIT DESCRIPTION**

A.M. aerial input via the common impedance of C16 to aerial tuning coils L10 (M.W.) and L11 (L.W.) which are connected in series with F.M. I.F. transformer secondary L9 in the input circuit of the frequency changer (V2, Mullard UGH61). This method of connection dispenses with A.M./F.M. change-over switches in this part of the circuit.  
 Section b of V2 operates as mixer, and section a as oscillator. Oscillator anode coils L14 (M.W.) and L15 (L.W.) are tuned by C29. Parallel trimming by C28 (M.W.) and C26, C27, C28 (L.W.); series tracking by C24 (M.W.) and C25 (L.W.). Reaction coupling from grid circuit via L12 (M.W.) and L13 (L.W.).  
 V3 (Mullard UF85) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C32, L18, L19, C33 and C40, L23, L24, C41.

**A.M. Intermediate frequency 470 ko/s.**

Diode section c of triple diode triode valve (V4, Mullard UABC80) functions as A.M. signal detector, and the audio frequency component in its rectified output is developed across R15, R16.

I.F. filtering by C43, R14 and the capacitance of the leads to chassis. The A.F. signal developed across R15, R16 is passed via S13, which closes on the A.M. bands, volume control R19, and C50 to grid of triode section d of V4, which operates as A.F. amplifier.

D.C. potential developed across R16 is fed back as bias to V2b and V3, giving automatic gain control.

Resistance-capacitance coupling by R21, C52 and R23 between V4d and pentode output valve V5 (Mullard UL41). Tone correction by C54, R28, C56 in V5 anode circuit and by negative feedback via R24 between V5 anode and V4d anode. C48, in conjunction with a three-position screw-type adjustment, provides three different levels of tone correction. In the A.M./F.M. position, C48 is shunted directly across R19 and gives treble cut in all positions of the waveband control, while in the A.M. or F.M. positions C48 is brought into operation only when the receiver is switched to A.M. or F.M. respectively.

Provision is made for the connection of an external low impedance speaker. A speaker muting switch S16 is provided to silence the internal speaker.

Filament voltage for the tuning indicator (T.I., Mullard DM70) is obtained from the volt-

age dropped across R27 in V5 cathode circuit. The grid circuit of the tuning indicator is connected via S14 to the D.C. load R17 for F.M. operation, or via S15 to the A.M. A.G.C. line for A.M. operation.

H.T. current is supplied by half-wave I.H.C. rectifying valve (V6, Mullard UY41). H.T. smoothing by choke L26 and electrolytic capacitors C57, C58. The valve filaments, together with ballast resistor R29, R30, R31, are connected in series across the mains input. R32 protects V6 from current surges. Mains R.F. filtering by C62.

**Operation on F.M.**

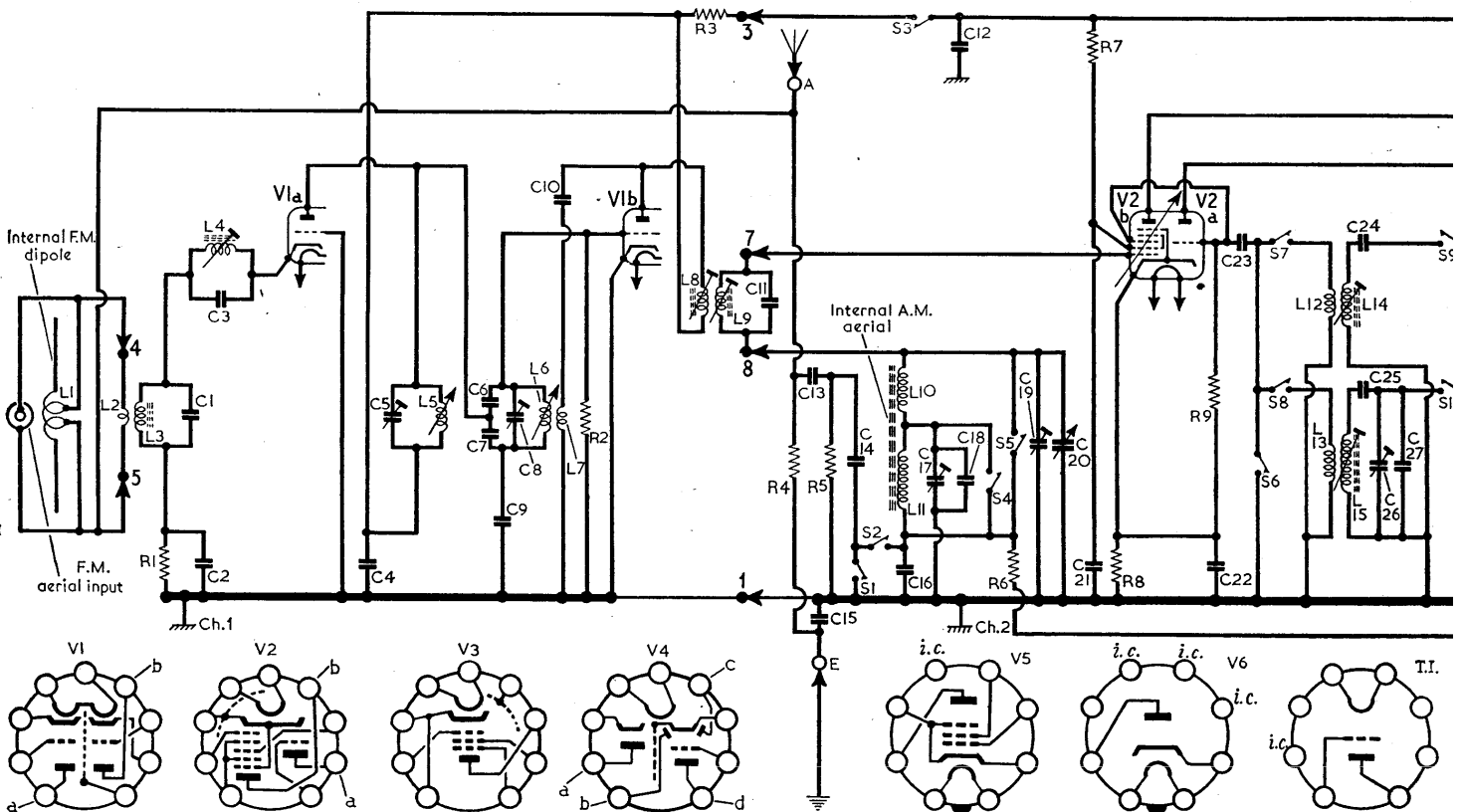
Co-axial 75 Ω F.M. aerial input via coupling transformer L2, L3 to R.F. amplifier, section a of V1 (Mullard UCG85). I.F. rejection by L4, C5.

Section b of V1 operates as oscillator/mixer valve with tuned oscillator grid circuit L6, C6, C7, C8. Reaction coupling from anode via C10, L7. Oscillator radiation is reduced by means of a bridge neutralizing circuit, formed by C6, C7, C9, and the inter-electrode capacitances of V1b, which prevents coupling between the oscillator and R.F. circuits. Oscillator tuning is by means of the ganged cores of L5, L6 which are cam-driven from the spindle of the tuning gang C20, C29.

V2b and V3 form the two-valve F.M. intermediate frequency amplifier, which is coupled by tuned transformers L8, L9, C11; C30, L16, L17, C31; and discriminator transformer C38, L20, L21, L22, C39 to diode sections a and b of V4 connected in a ratio detector discriminator circuit.

**F.M. intermediate frequency 10.7 Mc/s.**

The A.F. output of the ratio detector is developed across C42 and passed via R19 and C50 to V4d grid. Limiting is performed by the



# M./F.M. RECEIVER U243

ble Receiver for Operation from A.C. or D.C. Mains

"fly-wheel" effect of D.C. reservoir G45. Potential developed across D.C. load R17 is fed back as A.G.C. bias to V3 suppressor grid.

## COMPONENTS AND VALUES

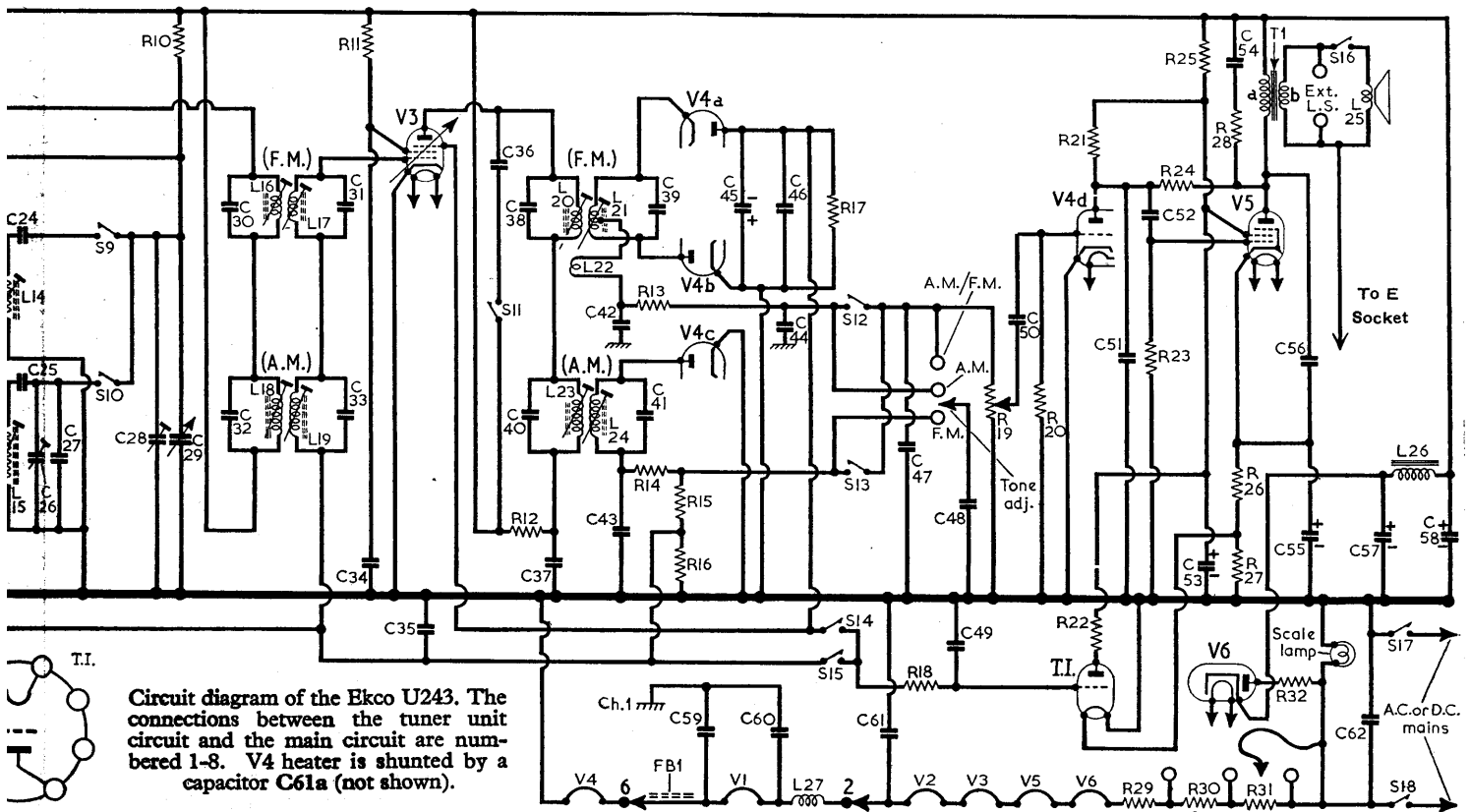
RESISTORS		Values	Locations
R1	V1a G.B. ...	220Ω	F3
R2	V1b C.G. ...	100kΩ	F3
R3	H.T. feed ...	4.7kΩ	F3
R4	A.M. aerial shunts	1MΩ	A2
R5	A.G.C. decoup. ...	1MΩ	G3
R7	V2b S.G. decoup. ...	10kΩ	G4
R8	V2 G.B. ...	180Ω	G4
R9	V2a C.G. ...	47kΩ	G4
R10	H.T. feed ...	68kΩ	G4
R11	V3 S.G. feed ...	82kΩ	F4
R12	H.T. feed ...	2.2kΩ	F4
R13	Part de-emphasis ...	39kΩ	F4
R14	I.F. stopper ...	100kΩ	E4
R15	A.M. detector load	470kΩ	B1
R16	D.C. load ...	470kΩ	F4
R17	D.C. load ...	33kΩ	E4
R18	T.I. decoupling ...	2.2MΩ	E3
R19	Volume control	1MΩ	D3
R20	V4d C.G. ...	10MΩ	E4
R21	V4d anode load	220kΩ	E4
R22	T.I. H.T. feed ...	470kΩ	D3
R23	V5 C.G. ...	680kΩ	E4
R24	Neg. feed-back ...	1.8MΩ	E4
R25	H.T. feed ...	10kΩ	E4
R26	V5 G.B. ...	180Ω	E4
R27	V5 G.B. ...	82Ω	E4
R28	Tone correction ...	22kΩ	D4
R29	Heater ballast ...	370Ω	C2
R30	Heater ballast ...	200Ω	C2
R31	Heater ballast ...	200Ω	C2
R32	V6 surge limiter ...	200Ω	C2

CAPACITORS		Values	Locations
C1	F.M. aerial tun. ...	12pF	F3
C2	Via cath. by-pass	0.001μF	F3
C3	F.M. I.F. filter	20pF	G3
C4	H.T. by-pass ...	500pF	F3
C5	F.M. R.F. trim.	30pF	F3
C6	F.M. osc. trimmers	6pF	F3
C7	F.M. osc. trimmers	30pF	G3
C8	F.M. osc. trimmers	12pF	G3
C9	F.M. osc. trimmers	22pF	G3
C10	F.M. osc. coup. ...	22pF	A1
C11	1st. F.M. I.F.T. tuning ...	22pF	F4
C12*	H.T. by-pass ...	0.011μF	F4
C13	A.M. aerial coup-ling	1,800pF	A2
C14	A.M. aerial coup-ling	0.01μF	A2
C15	Earth isolator ...	1,800pF	A2

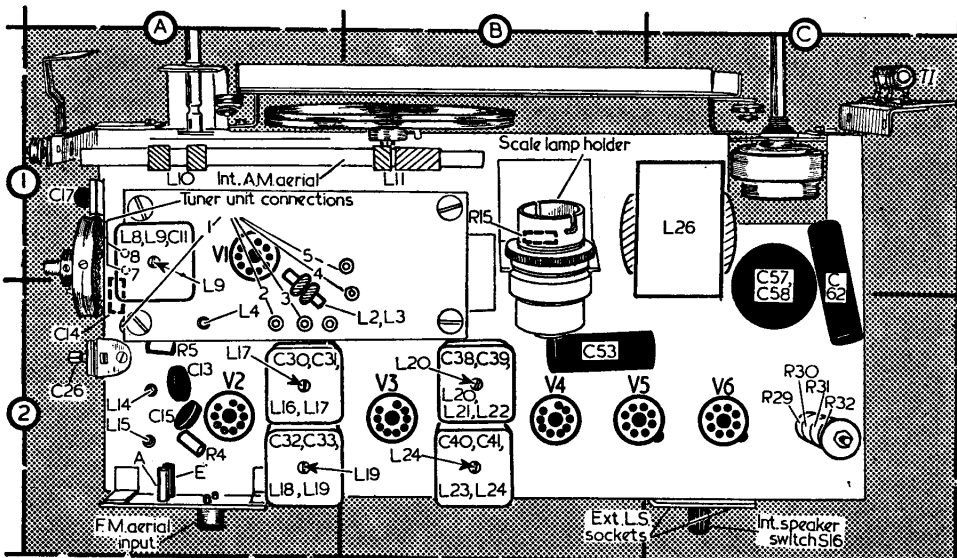
\*Two capacitors, 0.01μF + 0.001μF, in parallel.

Dealers are reminded that if the component numbers given in the component tables are used when ordering replacements, it is advisable to mention the fact on the order, as these numbers may differ from those used in the manufacturers' circuit.

CAPACITORS (Continued)		Values	Locations
C16	A.M. aerial coup.	2,500pF	G3
C17	L.W. aerial trim	40pF	A1
C18	L.W. aerial trim	50pF	G3
C19	M.W. aerial trim	—	F3
C20	Aerial tuning ...	—	F3
C21	V2b S.G. decoup.	0.01μF	G4
C22	V2 cath. by-pass	0.04μF	G4
C23	V2a C.G. ...	68pF	G4
C24	M.W. osc. tracker	470pF	G4
C25	L.W. osc. tracker	200pF	G4
C26	L.W. osc. trimmers	40pF	A2
C27	L.W. osc. trimmers	82pF	G4
C28	Osc. trimmer ...	—	F3
C29	A.M. osc. tuning	—	F3
C30	2nd F.M. I.F.T. tuning	22pF	A2
C31	1st F.M. I.F.T. tuning	17pF	A2
C32	1st A.M. I.F.T. tuning	100pF	A2
C33	V3 S.G. decoup.	100pF	A2
C34	V3 S.G. decoup.	0.01μF	F4
C35	A.G.C. decoup. ...	0.04μF	F4
C36	A.M. I.F.T. tun.	30pF	F4
C37	H.T. decoup.	0.01μF	F4
C38	3rd F.M. I.F.T. tuning	22pF	B2
C39	2nd A.M. I.F.T. tuning	30pF	B2
C40	2nd A.M. I.F.T. tuning	350pF	B2
C41	A.F. load ...	350pF	B2
C42	I.F. by-pass ...	100pF	E4
C43	I.F. by-pass ...	100pF	E4
C44	Part de-emphasis	0.001μF	F3
C45	D.C. reservoir ...	12μF	E4
C46	I.F. by-passes ...	100pF	E4
C47	I.F. by-passes ...	100pF	F3
C48	Tone correction	0.002μF	F4
C49	T.I. decoupling ...	0.01μF	D3
C50	A.F. coupling ...	0.01μF	D3
C51	I.F. by-pass ...	100pF	E4
C52	A.F. coupling ...	0.01μF	E4
C53	H.T. smoothing	8μF	B2
C54	Tone correction	0.02μF	D4
C55	V5 cath. by-pass	50μF	E4
C56	Tone correction	0.001μF	E4
C57	H.T. smoothing	50μF	C1
C58	H.T. smoothing	50μF	C1
C59	Heater by-pass capacitors	0.001μF	F3
C60	Heater by-pass capacitors	0.01μF	F3
C61a	Mains R.F. by-pass	0.01μF	G4
C62	Mains R.F. by-pass	0.1μF	H4



Circuit diagram of the Ekco U243. The connections between the tuner unit circuit and the main circuit are numbered 1-8. V4 heater is shunted by a capacitor C61a (not shown).



Plan illustration of the chassis, showing the majority of the tuner unit connections in A1 and A2. Connection 6 is shown in the underside illustration (location E4). A.M. internal aerial coils L10 and L11 in locations A1, B1 are mounted on a length of ferrite rod.

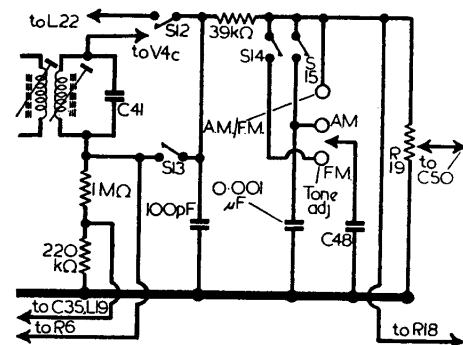


Diagram showing circuit differences as they appear in the A.M. and F.M. detector circuits of early versions of the receiver.

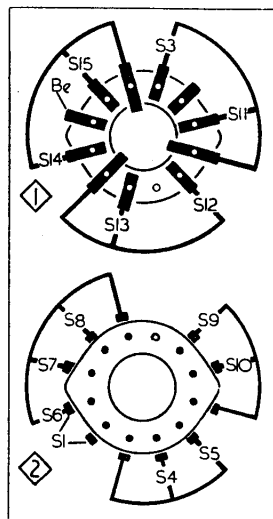
tuning indicator grid circuit either to the discriminator D.C. load or to the A.M. A.G.C. line.

**Drive Cord Replacement.**—About 36 inches of good quality flax fishing line, plaited and waxed, is required for a new gang drive, and about 20 inches of 7-strand steel wire is required for a new waveband indicator drive.

The gang drive drum should be turned to maximum capacitance and the drive cord should be run as shown in the sketch at the foot of column 5. The waveband indicator drive should be run as shown in the sketch at the foot of column 6.

Switch Table and Diagrams

Switches	L.W.	M.W.	F.M.
S1	—	—	o
S2	o	—	—
S3	—	o	—
S4	—	—	o
S5	—	—	o
S6	—	—	o
S7	—	—	o
S8	o	—	—
S9	—	o	—
S10	o	—	—
S11	—	o	—
S12	o	—	—
S13	—	o	—
S14	o	—	—
S15	o	—	—



Diagrams of the waveband switch units, as seen in the direction indicated by the numbered arrows in the under-chassis illustration.

OTHER COMPONENTS	Approx. Values (ohms)	Locations
L1	Int. F.M. dipole ...	—
L2	F.M. aerial coup. coils ...	A1
L3	F.M. I.F. rejector ...	G3
L4	F.M. R.F. coil ...	F3
L5	F.M. osc. coils ...	G3
L6	F.M. osc. coils ...	G3
L7	F.M. osc. coils ...	G3
L8	1st F.M. I.F.T. { Pri. ...	A1
L9	1st F.M. I.F.T. { Sec. ...	A1
L10	Int. A.M. aerial coils ...	A1
L11	Int. A.M. aerial coils ...	B1
L12	A.M. osc. reaction coils ...	G4
L13	A.M. osc. reaction coils ...	G4
L14	A.M. osc. tuning coils ...	G4
L15	A.M. osc. tuning coils ...	G4
L16	2nd F.M. I.F.T. { Pri. ...	A2
L17	2nd F.M. I.F.T. { Sec. ...	A2
L18	1st A.M. I.F.T. { Pri. ...	A2
L19	1st A.M. I.F.T. { Sec. ...	A2
L20	3rd F.M. I.F.T. { Pri. ...	B2
L21	3rd F.M. I.F.T. { Sec. ...	B2
L22	3rd F.M. I.F.T. { Tert. ...	B2
L23	2nd A.M. I.F.T. { Pri. ...	B2
L24	2nd A.M. I.F.T. { Sec. ...	B2
L25	Speech coil ...	—
L26	H.T. Smoothing choke ...	C1
L27	Heater R.F. choke ...	F3
T1	O.P. trans. { a ...	E3
S1-S15	Waveband switches	G3
S16	Int. L.S. switch ...	D4
S17, S18	Mains sw., g'd R19	D3

GENERAL NOTES

**Switches.**—S1-S15 are the waveband and A.M./F.M. change-over switches, ganged in two rotary units beneath the chassis. These units are identified in the underchassis illustration, where the numbered arrows indicate the direction in which they are viewed in the diagrams of the units in column 2. The associated switch table below the diagrams gives the switch operations for the three control settings starting with the control in its fully anti-clockwise position. A dash indicates open, and C, closed.

S16 is the internal speaker muting switch, mounted between the external speaker sockets in location C2.

S17, S18, are the Q.M.B. mains switches ganged with the volume control R19.

**Scale Lamp.**—This is a 230-250 V, 15 W pygmy lamp with a bayonet cap base.

**Modifications.**—Differences between the sample receiver on which this Service Sheet was prepared and earlier models are as follows.

A 20pF capacitor was connected between the lower end of L2 and chassis. C12 was an 0.01μF capacitor. R28, C54 were not fitted. An 0.001μF capacitor was connected in series between R24 and the junction of R28 and V5 anode. R22 was 220 kΩ.

In the A.M. detector and F.M. discriminator circuits there were many differences which can be seen in the diagram of the original section of the circuit above. These differences are mainly centred round switches S14, S15, which are employed here in the 3-position tone adjustment circuit. In later circuits, as seen in the diagram overleaf, these switches are used to connect the

VALVE ANALYSIS

Valve voltages and currents given in the table below are those measured in our sample receiver when it was operating from A.C. mains of 230 V. The receiver, except where otherwise indicated, was tuned to the high wavelength end of M.W., and there was no signal input.

Voltages were measured with an Avo Electronic Test Meter, and as this instrument has a high internal resistance, allowance should be made for the current drawn by other types of meter. Chassis was the negative connection in every case.

Valve	Anode		Screen		Cath.
	V	mA	V	mA	
V1 UCC85*	135	4.5	—	—	1.3
V2 UCH81	135	4.0	—	—	—
V3 UF85	48	2.2	—	—	2.8
V4 UAB80	195	5.5	130	7.4	2.8
V5 UL41	175	7.4	50	2.5	—
V6 UY41	—	—	—	—	—
T.I. DM70	60	0.4	—	—	—
	180	37.0	130	10.0	8.0
	150†	—	—	—	215.0‡
	90	—	—	—	—

\*Switched to F.M. †A.C. reading, each anode. ‡Cathode current 67mA.

DISMANTLING

**Removing Chassis.**—Remove volume and tuning control knobs (grub screws) from front of cabinet, and waveband knob (grub screw) from side of cabinet;

remove plastics runners from base of cabinet (four wood screws), and unscrew four chassis bolts thus revealed;

unclip white and pink internal F.M. aerial leads from their terminations on the tuner unit;

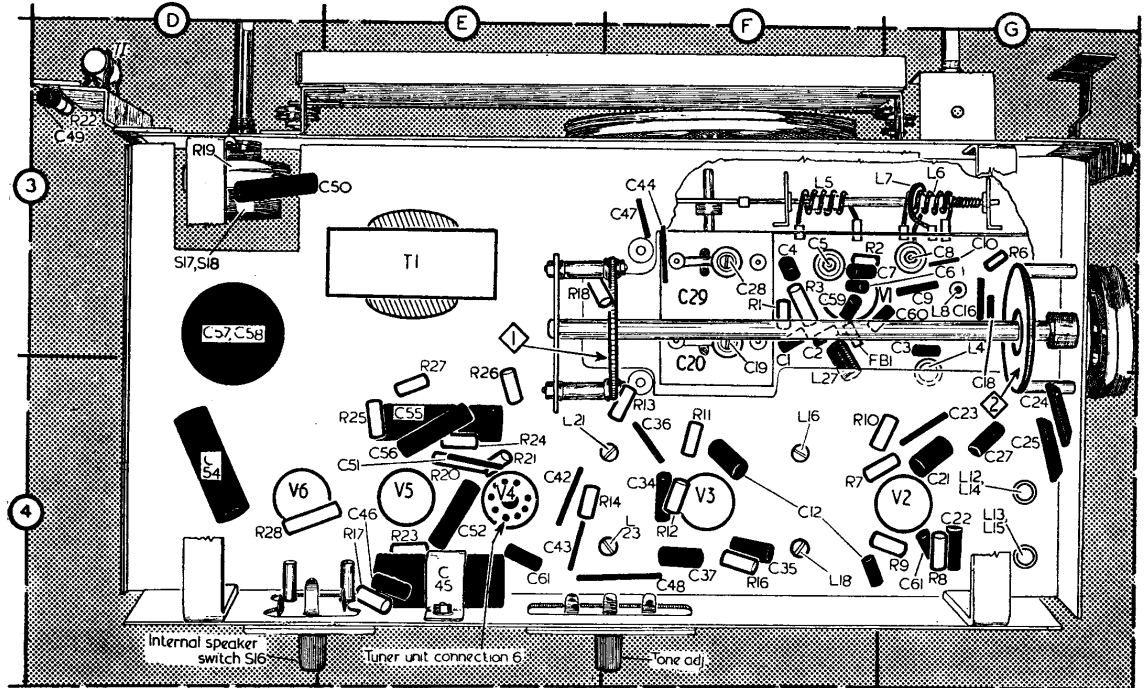
unsolder leads from speech coil tags on speaker, and withdraw chassis.

CIRCUIT ALIGNMENT

Remove chassis from cabinet and support it on its ballast resistor end on the bench. Remove tuning scale from cabinet (held by three springs and wood block), and place it in position over the control spindles.

**Equipment Required.**—An A.M. signal generator covering the range of 140 kc/s to 1.5 Mc/s; an F.M. signal generator covering the F.M. intermediate frequency of 10.7 Mc/s and the frequency range of 86-100 Mc/s, with a deviation of at least ±25 kc/s (if an F.M. signal

Underside illustration of the chassis. The chassis is shown broken in locations F3 and G3 to reveal the F.M. tuning coils L5, L6 and L7. C61 in location B4 is actually C61a.



generator is not available, the instructions given under "F.M. Alignment using A.M. Generator" should be used; an output meter with an internal resistance of  $3\ \Omega$ ; a  $0.100\ \mu\text{A}$  D.C. microammeter; two  $220\ \text{k}\Omega$  resistors.

**F.M. I.F. Stages.**—Switch receiver to F.M. and tune it to  $87\ \text{Mc/s}$ . Connect output meter across speech coil tags on speaker and disconnect internal F.M. aerial. Connect output of F.M. signal generator, via an  $0.01\ \mu\text{F}$  capacitor in each lead, to control grid (pin 2) of V3 and to chassis.

1.—Feed in a  $10.7\ \text{Mc/s}$  signal deviated by  $\pm 25\ \text{kc/s}$  and adjust the core of L20 (location reference B2) for maximum output.

2.—Connect  $220\ \text{k}\Omega$  resistors in series across R17, and connect microammeter between the junction of these resistors and the junction of C42, R13. Adjust the core of L21 (F4) for zero current. Disconnect resistors and microammeter.

3.—Transfer F.M. generator "live" lead, with isolating capacitor, to control grid (pin 2) of V2. Adjust the cores of L17 (A2) and L16 (F4) for maximum output.

4.—Check that the outputs at  $10.6\ \text{Mc/s}$  and  $10.8\ \text{Mc/s}$  are equal. A slight adjustment should be made to the core of L21 if any inequality exists.

5.—Transfer F.M. signal generator live lead with isolating capacitor, to cathode (pin 8) of V1a and chassis. Adjust the cores of L9 (A1) and L8 (G3) for maximum output.

6.—Transfer signal generator leads to F.M. aerial socket and adjust the core of L4 (A2) for minimum output.

**A.M. I.F. Stages.**—Switch receiver to M.W. and tune receiver to  $545\ \text{kc/s}$ . Connect output of spot-frequency signal generator, via an  $0.01\ \mu\text{F}$  capacitor in each lead, to control grid (pin 2) of V2 and to chassis.

7.—Feed in a  $30\%$  modulated  $470\ \text{kc/s}$  signal and adjust the cores of L24 (B2), L23 (F4),

L19 (A1) and L18 (F4) for maximum output.

**F.M. R.F. and Oscillator Stages.**—Check that with the gang at maximum capacitance the cursor coincides with the calibration marks at the high wavelength end of the M.W. and L.W. bands, and that the F.M. tuning plunger, which is driven by a cam on the gang spindle, projects from its screening can by  $\frac{1}{2}$  in overall.

8.—Switch receiver to F.M. and tune it to  $94\ \text{Mc/s}$ . Set C8 (G3) to maximum capacitance, and adjust C5 (F3) to mid-capacitance. With F.M. signal generator connected to F.M. aerial socket, feed in a  $94\ \text{Mc/s}$  signal and adjust C8 to the first peak obtained on unscrewing the trimmer from maximum capacitance.

9.—Adjust C5 for maximum output. Readjust C8 for maximum output.

10.—Check calibration at  $98\ \text{Mc/s}$  and  $90\ \text{Mc/s}$  and adjust position of cam on gang shaft if necessary to correct errors. Repeat operation 9.

**A.M. R.F. and Oscillator Stages.**—Connect spot-frequency signal generator, via a standard dummy aerial, to A and E sockets.

11.—Switch receiver to M.W. and tune it to  $500\ \text{m}$ . Feed in a  $500\ \text{m}$  ( $600\ \text{kc/s}$ ) signal and adjust the core of L14 (A2) for maximum output.

12.—Tune receiver to  $214.3\ \text{m}$ , feed in a  $214.3\ \text{m}$  ( $1,400\ \text{kc/s}$ ) signal and adjust C28 (F3) for maximum output. Repeat this adjustment, and operation 11.

13.—Retune receiver to  $500\ \text{m}$ , feed in a  $500\ \text{m}$  ( $600\ \text{kc/s}$ ) signal and adjust the inductance of L10 (A1) for maximum output by sliding it along the ferrite rod.

14.—Retune receiver to  $214.3\ \text{m}$ , feed in a  $214.3\ \text{m}$  ( $1,400\ \text{kc/s}$ ) signal and adjust C19 (F3) for maximum output. Repeat this adjustment and operation 13.

15.—Switch receiver to L.W. and tune it to  $2,000\ \text{m}$ . Feed in a  $2,000\ \text{m}$  ( $150\ \text{kc/s}$ ) signal and

adjust the core of L15 (A2) for maximum output.

16.—Tune receiver to  $1,000\ \text{m}$ , feed in a  $1,000\ \text{m}$  ( $300\ \text{kc/s}$ ) signal and adjust C26 (A2) for maximum output. Repeat this adjustment and operation 15.

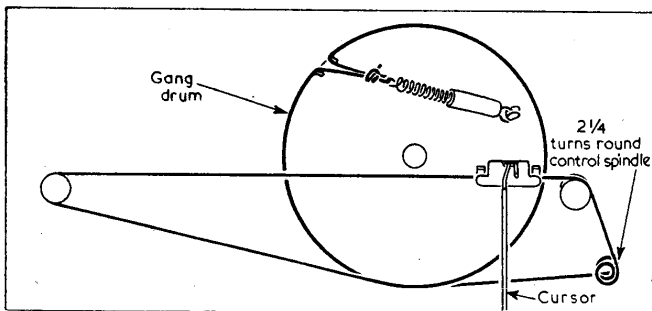
17.—Retune receiver to  $2,000\ \text{m}$ , feed in a  $2,000\ \text{m}$  ( $150\ \text{kc/s}$ ) signal and adjust the inductance of L11 (B1) for maximum output by sliding the coil along the ferrite rod.

18.—Retune receiver to  $1,000\ \text{m}$ , feed in a  $1,000\ \text{m}$  ( $300\ \text{kc/s}$ ) signal and adjust C17 (A1) for maximum output. Repeat this adjustment and operation 17.

**F.M. Alignment Using A.M. Generator.**—When using an A.M. signal generator for F.M. alignment an unmodulated signal should be used throughout, and the R.F. and oscillator operations 8-10 should be made for maximum voltage output across R17, measured on a high resistance  $0.10\ \text{V}$  D.C. voltmeter.

**Sensitivity Figures.**—Not more than  $70\ \text{mV}$  of  $10.7\ \text{Mc/s}$  signal, deviated by  $\pm 25\ \text{kc/s}$ , should be required at V3 control grid to produce an output of  $500\ \text{mW}$  across T1 secondary winding. Not more than  $5.5\ \text{mV}$  of signal at V2 control grid, and not more than  $2\ \text{mV}$  of signal at V1b cathode should be required to produce a  $500\ \text{mW}$  output.

**Response Curves.**—Check that with the signal generator output connected to V3 control grid and to chassis, the outputs at  $10.45\ \text{Mc/s}$  and at  $10.95\ \text{Mc/s}$  are not less than half that at  $10.7\ \text{Mc/s}$ . Check that with the generator connected to V2 control grid and chassis, the outputs at  $10.6\ \text{Mc/s}$  and  $10.8\ \text{Mc/s}$  are not less than half that at  $10.7\ \text{Mc/s}$ . Finally, check that with the generator connected to V1a cathode and chassis, the outputs at  $10.61\ \text{Mc/s}$  and  $10.79\ \text{Mc/s}$  are not less than half that at  $10.7\ \text{Mc/s}$ .



Sketch of the gang drive cord system as seen from the front of an upright chassis with the gang at maximum capacitance.

Sketch of the waveband indicator drive as seen from the waveband control side of an upright chassis, with the control switched to F.M.

