

"TRADER" SERVICE SHEET

1325

# MURPHY BA228

Covering also Model B229

**E**MPLYING an internal frame aerial, the Murphy BA228 is a six-valve (plus two metal rectifiers), 2-band portable receiver designed to operate from a combined all-dry battery or A.C. mains of 200-250V, 50c/s. The wavebands covered are 187-540m and 1,000-2,000m. Model B229 is a similar receiver housed in an identical cabinet, but designed to operate from a combined all-dry battery only.

The circuits of both receivers are very much alike in most respects, and our diagram shows them both completely. Differences are indicated in the main body of the diagram by using thick lines to indicate wiring that is present only in the BA228, while dotted lines indicate that it is present only in the B229. The A.C. mains power supply circuit for the BA228 is shown separately on the right of the main diagram.

Release date both models: September 1954. Original prices: BA228, £17 5s; B229, £14 16s 3d. Purchase tax and battery extra.

## CIRCUIT DESCRIPTION

The frame aerial L1 is switched directly across the tuning capacitor C5 or to a tapping on L.W. coil L2, and precedes heptode frequency changer valve V1 operating with electron coupling. Provision is made for connection to an external aerial via socket A. This socket is isolated by C1 in model BA228 only.

Oscillator grid coils L5 M.W. and L6 L.W. are tuned by C14. Parallel trimming by C13 and C15 on M.W. and C16 and C17 on L.W. Series tracking by C11 M.W. and C11, C12 on L.W. Reaction coupling from oscillator anode via L7 and L8.

I.F. amplifying valve V2 is a variable-mu R.F. pentode operating with tuned transformer couplings C8, L3, L4, C9 and C20, L9, L10, C21. These transformers are hermetically sealed units and plugs are fitted over the core adjustment heads.

### Intermediate frequency 470 Kc/s.

Diode signal detector is part of diode-pentode valve V3. Audio frequency component in its rectified output is developed across the volume control R8, which also functions as the diode load, and is passed via C25 to the pentode section of V3, which operates as the A.F. amplifier. Anode circuit decoupling to V3 H.T. supply is provided by R14, C28 in model BA228 only, as indicated by the heavy lines. To obtain the maximum reduction of hum when working from A.C. mains supply, the volume control R8 grid leak R9 and screen bypass capacitor C27 in the BA228 are returned to chassis via the junction of R12 with R13. These two resistors form a potential divider across the filament supply to V3 and again as indicated by the heavy lines they are present only in model BA228; in model B229

R8, R9 and C27 are returned direct to the chassis. A feed-back circuit, comprising C29, R16, C30 and R10 from V3 anode circuit to chassis and control grid circuit, provides additional hum reduction.

### Output Stage

Output from V3 anode is resistance-capacitance coupled via R15, C31, R21 to one-half (V5) of the push-pull output stage V5, V6 and by R15, C31, C32, R19 to V4, which has anode and screen joined to operate as a triode. V4 functions as a phase inverter and is resistance-capacitance coupled via R20, C34, R22 to the other half of the push-pull output stage V6.

The driving circuits for the output stage are balanced, and allowance is made for the slight additional gain introduced by V4 by suitably selecting the values of the coupling capacitors. C33, from the junction of C34 with R22 to control grid of V4, provides feed-back which effectively cancels any I.F. component introduced in the phase-inverter stage by the A.G.C. diode of V4.

### Automatic Gain Control

Automatic gain control of V1 and V2 is achieved by coupling the I.F. amplifier anode to V4 diode via C24, and the resultant rectified output is developed as a D.C. potential across R18. This D.C.

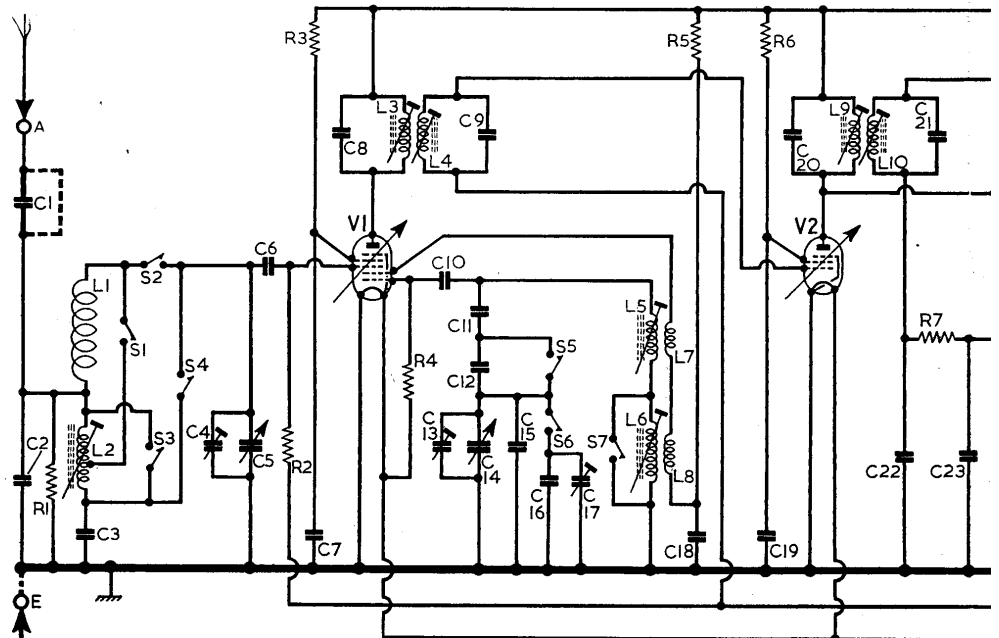
potential is then fed via filter circuit R17, C26 as A.G.C. bias to V1 and V2 control grid circuits.

### Power Supplies

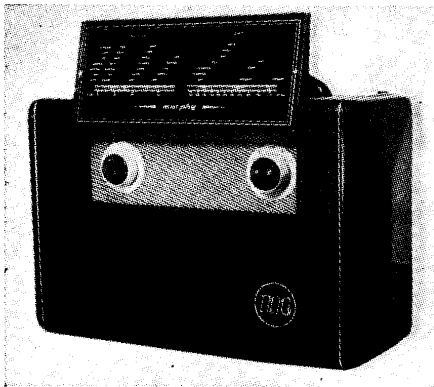
As explained earlier, our circuit diagram shows the circuits of the battery-only model B229 and the mains/battery version BA228. With the exception of the separated mains-derived power circuit on the extreme right our diagram shows the circuits of both models all the way through.

Most of the circuit is identical in both models, and it is then drawn in the normal manner, but where differences occur they are indicated either by thickening the line or by breaking it into dots. A thickening of the line indicates that the wiring represented (and components included in it), is present only in the mains/battery model, while the breaking of a line into dots indicates that it is present only in the battery-only model. Our chassis line is represented as usual by a very heavy line which is of course common to both versions.

The separated mains power circuit on the right is drawn normally, but the complete power circuit applies to the mains/battery model only, as indicated in the diagram. In this model, the complete receiver circuit is shown if the breaks between the two sections of the diagram are bridged.



Circuit diagram of Murphy BA228 and B229 receivers. Components and wiring shown dotted refer to model B229 only, and those shown in thicker lines refer to model BA228 only. All remaining connections are common to both receivers. The power supply circuit on the right applies to the BA228 receiver only.



Appearance of both models.

In the battery-only model, the H.T. negative lead from the battery goes (via dotted lines) to **R23**, and current flowing through **R23** to chassis produces a voltage drop which provides grid bias for the output valves. Their grid resistors **R21**, **R22** go to the H.T. negative plug. The H.T. positive lead goes via **S8** to the H.T. positive line. The L.T. negative lead goes directly to chassis; and the L.T. positive lead goes via **S9** to the filaments.

In the mains/battery version BA228, power supplies for battery operation are obtained from the same sources as they are in the B229, but they take a different route. For A.C. mains operation, of course, power supplies are obtained from the separately drawn mains power circuit on the right.

Here the H.T. supply is taken from secondary winding **c** on the mains transformer **T2** and rectified by **MR2** in the negative side of the circuit, which goes to

COMPONENT TABLES

Resistors			Capacitors			C4			Colls*			Transformers*			Miscellaneous			
R1	10kΩ	A1	C1	1,800pF	H4	C4	35pF	H3	C39	2,000μF	C1	T1	460-0	a	E3	MR1	011L999*	G4
R2	470kΩ	B1	C2	3,900pF	A1	C5	523pF*	H4	C40	32μF	F3	T2	400-0	b	D1	MR2	15C997*	E3
R3	180kΩ	B1	C3	73pF	A1	C6	100pF	B1	L1	—	—		—	c		S1-S7	—	A1
R4	27kΩ	B2				C7	0.04μF	B2	L2	1.7	—		23-0	a		S8-S13	—	D1
R5	27kΩ	A2				C8	68pF	B2	L3	32.5	A2		1.3	b		Scale	lamps	—
R6	39kΩ	F4				C9	68pF	B2	L4	18.3	B1		460-0	c		12-14 V,	0.75 W.	
R7	22kΩ	F3				C10	82pF	A2	L5	18.3	B1		—	—				
R8	1MΩ	D1				C11	490pF	A2	L6	5.0	H4		—	—				
R9	10MΩ	F3				C12	390pF	A1	L7	9.5	H4		—	—				
R10	2.2MΩ	F4				C13	35pF	H3	L8	—	H4		—	—				
R11	2.7MΩ	F3				C14	523pF*	H3	L9	18.3	C1		—	—				
R12	1kΩ	F3				C15	10pF	B1	L10	16.0	C1		—	—				
R13	222Ω	F4				C16	100pF	B2	L11	2.7	—		—	—				
R14	100kΩ	F3				C17	35pF	A2	L12	5.5	G3		—	—				
R15	1MΩ	F4				C18	0.04μF	B2										
R16	1MΩ	F4				C19	0.04μF	F4										
R17	1MΩ	F4				C20	68pF	C2										
R18	1MΩ	E4				C21	100pF	C2										
R19	10MΩ	E4				C22	100pF	F3										
R20	680kΩ	F4				C23	100pF	F3										
R21	1.5MΩ	E4				C24	10pF	F4										
R22	1.5MΩ	E3				C25	0.04μF	F4										
R23†	820Ω	—				C26	0.04μF	G4										
R24	6.5Ω	D1				C27	0.04μF	F4										
R25	470kΩ	F4				C28	0.1μF	F4										
R26	470Ω	C1				C29	1,800pF	F4										
R27	270Ω	D1				C30	0.002μF	E4										
R28	1.5kΩ	F3				C31	1,800pF	F4										
						C32	120pF	E4										
						C33	100pF	E4										
						C34	0.02μF	E4										
						C35	32μF	G3										
						C36	0.003μF	E4										
						C37	0.1μF	E3										
						C38	1,000μF	C1										

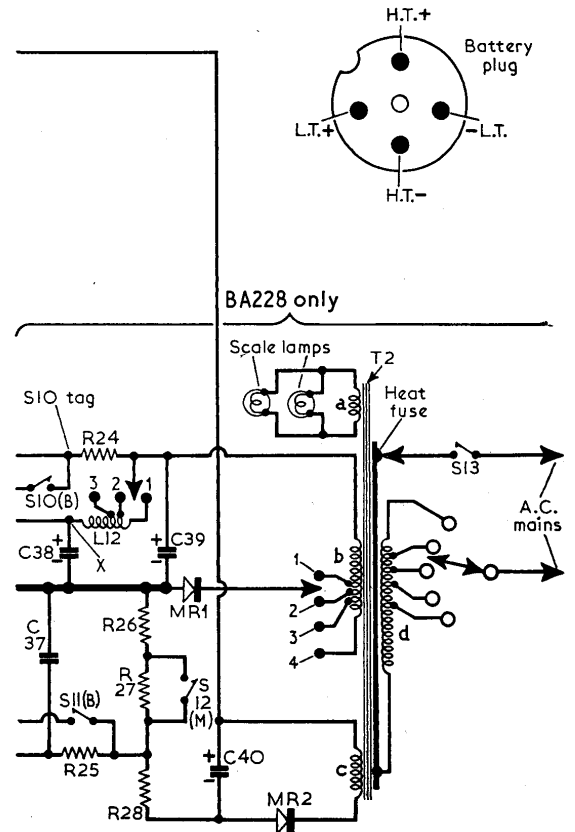
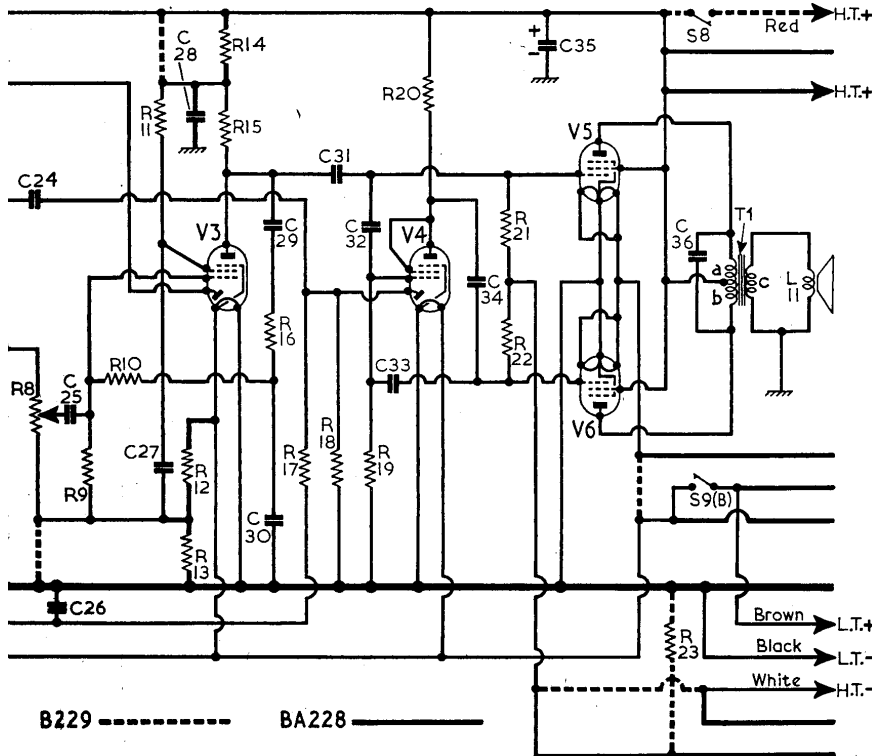
†In model B229 only; not shown in our chassis illustrations. \*\*"Swing" value minimum to maximum. ‡Westinghouse. \*Approximate D.C. resistance in ohms.

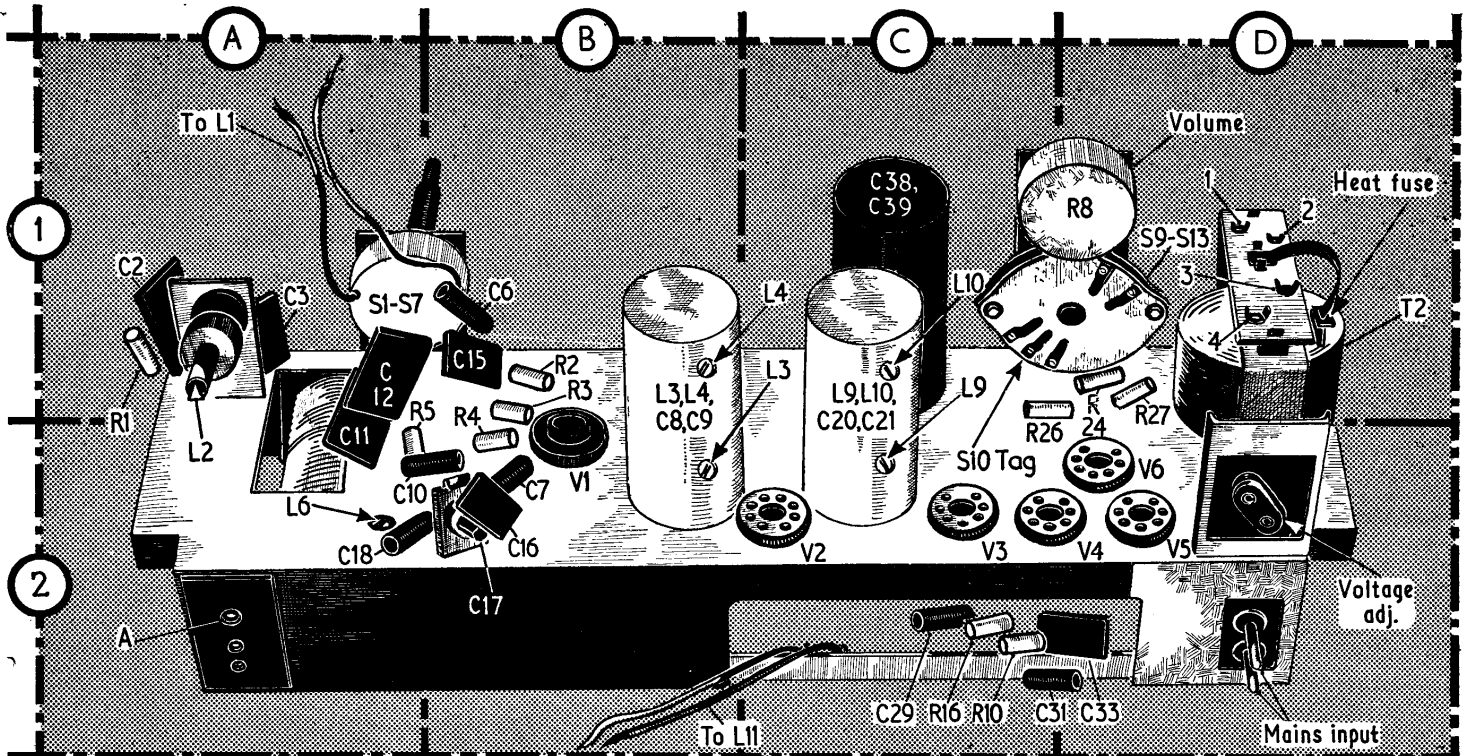
chassis via bias resistors **R28**, **R27**, **R26**. These and electrolytic capacitors **C40**, **C35** provide the main smoothing.

Filament current is obtained from another secondary winding **b**, which is tapped to permit accurate adjustment of the filament voltage. A metal rectifier **MR1** again is in the negative side of the circuit, and smoothing is provided by **L12**

(for **V1**, **V2**, **V3** and **V4** filaments) and **C39**, **C38**. **L12** is tapped for accurate adjustment, which is fairly critical. **S9** and **S10** are then open, and current for the output valve filaments is taken via **R24**.

Grid bias for the output valves is obtained from the drop along **R26** at the junction of **R27** and **R28**, **S12** being closed (Continued col. 1 overleaf)





Plan view of chassis. Tappings on T2, used in adjusting the L.T. voltage, are shown in D1. The mounting of V1 is inverted and the valve is inserted from the underside of the chassis.

#### Circuit Description—continued

for mains operation. S11 is open, and C37, R25 decouple the grid circuit. Grid circuit of V3 is returned via R9 to the potential divider R12, R13 on mains or battery.

For battery operation, as indicated by the suffix letters on them, switches S9, S10 and S11 close, while S12 opens. The H.T. negative lead then goes via S11 (B) to the potential divider R27, R26 to provide grid bias for the output valves, while the H.T. positive lead goes directly to the H.T. positive line.

The L.T. negative lead goes directly to chassis, but the L.T. positive lead goes to the junction of two switches. S9 connects it to the filaments of V1-V4, and S10 connects it to those of V5 and V6. The dotted line shown across these two switches is not present in the BA228.

#### CIRCUIT ALIGNMENT

The complete alignment of both I.F. and R.F. circuits can be carried out with the chassis in the cabinet, provided that the alignment of the scale cursors and drive cords has been checked as explained under "Drive Cord Replacement." A non-metallic trimming tool must be used, and all cores should be adjusted to the peak nearer to the adjusting end of the former.

For output indication, connect a high-resistance 0-2V A.C. voltmeter across the secondary of T1 and turn receiver volume control to maximum. Then carry out the alignment instructions given below ensuring that, as circuits are brought into tune, the receiver output is maintained, by reduction of signal generator output, at 0.4V. If the output reading is greater than 0.4V the A.G.C. circuit will become operative and make alignment difficult.

#### I.F. Alignment

The I.F. transformers are hermetically sealed, and the adjustment head openings are closed by rubber plugs. The plugs may be removed, but care must be taken to see that they are removed only during the alignment process, and then for only the shortest possible time. To carry out the alignment process, make the adjustments given below, but do not re-adjust the secondaries after adjusting the primaries, or the response curve will be incorrect.

1.—Connect the signal generator, via a 0.001 $\mu$ F capacitor, to the control grid (pin 6) of V2. Switch receiver to L.W., turn tuning gang to maximum capacitance, then feed in a 470 kc/s signal and adjust cores L10 (C1), and then L9 (C1), to give maximum output on meter.

2.—Transfer live signal generator lead to control grid (pin 6) of V1. Switch receiver to M.W. and, with tuning gang still at maximum, feed in a 470 Kc/s signal and adjust cores of L4 (C1), and then L3 (C1), for maximum output.

#### R.F. Alignment

Complete R.F. alignment can be carried out only with the chassis in the cabinet and with the frame aerial correctly connected. The signal generator should be connected, via dummy aerial, to the aerial socket A in location reference A2. Check drive cord and scale pointer alignment as explained in "Drive Cord Replacement," then carry out the following instructions.

1.—Switch the receiver to M.W., turn tuning gang to 500m, feed in a 600 kc/s signal and adjust core of oscillator coil L5 (H4) for maximum output on meter.

2.—Turn tuning gang to 200m, feed in a 1,500 kc/s signal and adjust capacitors C13 and C4 (H3) for maximum output.

3.—Switch the receiver to L.W., turn

tuning gang to 1,900m, feed in a 157.9 kc/s signal and adjust cores of L6 (A2) and L2 (A2) for maximum output.

4.—Turn tuning gang to 1,000m, feed in a 300 kc/s signal and adjust C17 (B2) for maximum output.

5.—Repeat all R.F. alignment operations for optimum results.

#### GENERAL NOTES

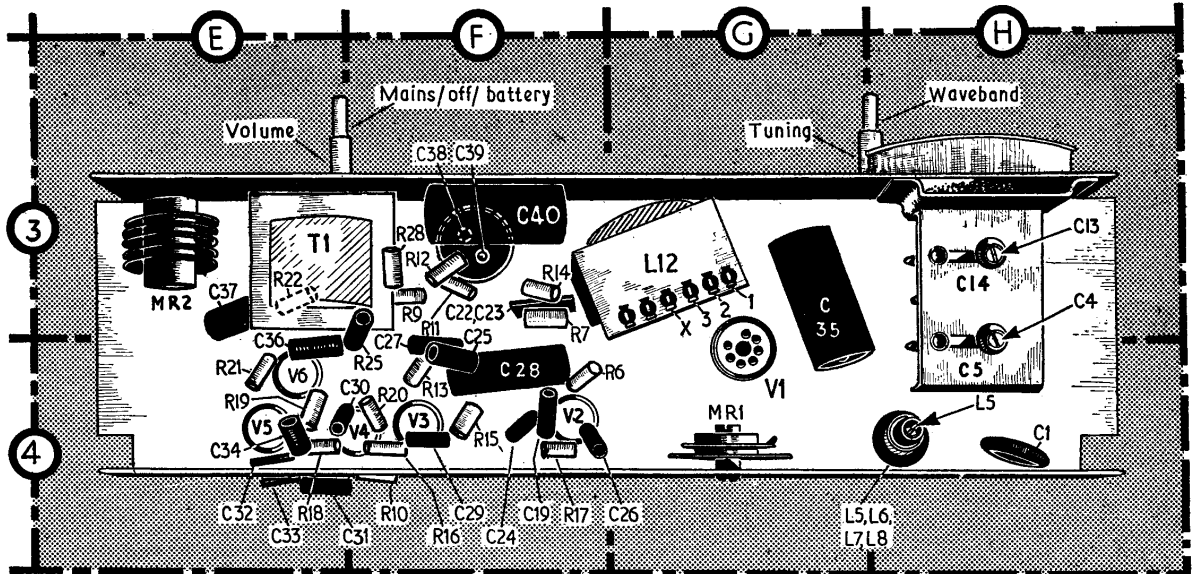
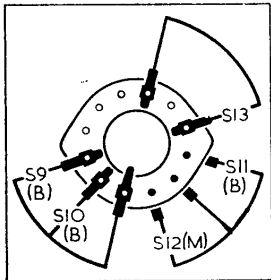
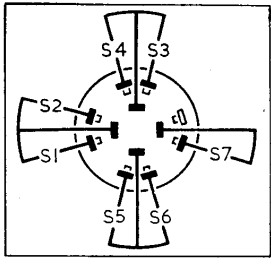
**Switches.**—S1-S7 are the waveband switches, ganged in a single rotary unit on the chassis deck in location reference A1. These waveband switches operate as follows: S2, S3, S5 and S7 close for M.W. operation, and S1, S4, S6 close for L.W. operation.

S9-S13 are the mains/battery and on/off switches ganged in a single rotary unit on the chassis deck in location reference D1.

These two units are indicated in our plan view of the chassis, and they are shown in detail in the diagrams in col. 4, where they are drawn as seen when viewed from the rear of the chassis. S9-S12 have a suffix (M) for mains or (B) for battery to indicate which closes for each mode of operation.

**Filament Voltage Adjustment.**—In model BA228, when any component associated with the filament circuit, or any valve, is replaced, the filament line voltage must be checked and, if necessary, adjusted. To perform this check, use a high resistance D.C. voltmeter, and with chassis as the negative connection carry out the following instructions.

1.—Measure the voltage at "S10 tag" (C2) which should be between 1.3V and 1.4V. If the reading is outside these limits, adjust the tapping on winding b on T2 (supplying MR1) to give a reading as near as possible to 1.35V. (These tappings on T2 are numbered 1-4 in location reference D1, and in the circuit



Left: Diagrams of the switch units showing them as seen when viewed from the rear of the chassis. Right: Underside illustration of chassis showing position of MR1 and L12. The unidentified tags on L12 are those referred to as carrying H.T. current.

diagram.) Care must be taken that no contact is made with the heat fuse, which is very close to the tapping tags.

2.—Measure the voltage at tag X on L12, which should be between 1.3V and 1.4V. If the reading is outside these limits, adjust the tapping on L12 to give a reading as near as possible to 1.35V. (Theseappings on L12 are numbered 1-3 in circuit diagram, and in location reference G3 adjacent to tag X.) Care must be taken that no contact is made with H.T. tags on L12 tag panel.

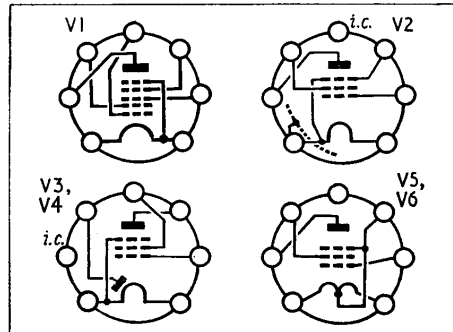
3.—If after fitting a replacement rectifier MR1, the L.T. voltage is too high and cannot be corrected by either of the foregoing adjustments, a 22Ω resistor, rated at 6W, must be connected between the connecting tag on MR1 and tag 1 on L12, and then the voltage adjusted accordingly.

**Battery.**—A combined 90V (H.T.) and 1.5V (L.T.) battery is required for either model, and types recommended by the makers are: Drymax 503; Ever Ready B103; G.E.C. BB503; Siemax S103; or Vidor L5507.

**DRIVE CORD REPLACEMENT**

Two interconnected drive cords are fitted, and to replace either of these a length of nylon braided cord of approximately 43in or 34in is required. These cords are held together by a clip and details of fitting are illustrated in col. 5. The tension springs shown in the illustration should be extended to 5/8in.

To align the two cords turn tuning gang to maximum capacitance, which occurs before the stop is reached, when the eyelet fitted to the main drive cord should correspond with the 0.2 mark on the diagonal scale attached to the chassis. With the chassis in the cabinet, and the two drive cords held together by the clip, the M.W. scale cursor should coincide with the right-hand edge of the 540m mark on the glass tuning scale. If it does not, then the cursor drive cord should be adjusted by moving it through the clip holding it to the main drive cord.



Above: Diagram of valve bases viewed from free ends of the pins. Below: Illustration of the drive cord system as seen from the front.

**VALVE ANALYSIS**

Valve voltages given in the table below are those derived from the manufacturers' information. The receiver was switched to M.W., but there was no signal input. In the case of the BA228, it was

operating from A.C. mains of 240V, and in the case of the B229, from a new combined H.T./L.T. battery. Voltages were measured on the 100V range of a 20,000 ohms-per-volt meter, chassis being the negative connection in each case.

Total consumption is given by the makers as 7 watts from the mains in the case of the BA228; for the B229, H.T. current is given as 10mA, and L.T. current as 225mA. Battery consumption for model BA228 will be similar.

Valve	Model BA228		Model B229	
	Anode (V)	Screen (V)	Anode (V)	Screen (V)
V1 IC2 { osc. mixer	33	—	33.0	—
V2 1F1 ..	87	61	82.5	54.0
V3 1FD1 ..	87	70	82.5	63.0
V4 1FD1 ..	7	18	16.0	29.0
V5 1P1* ..	28	28	36.0	36.0
V6 1P1* ..	86	87	81.5	82.5
	86	87	81.5	82.5

\*Negative bias voltage, developed in H.T. negative lead to chassis, is: 7.5 V (B229), 6.2 V (BA228).

